



Analysis of Mechanical Parameters Using End-Diastolic Measurements

Ruth Arís

**Barcelona Supercomputing Center
Centro Nacional de Supercomputación
Spain**

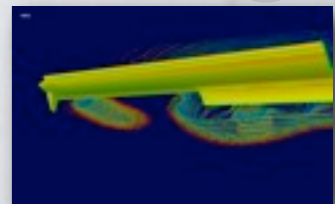
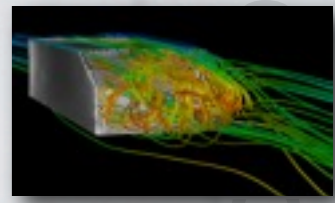
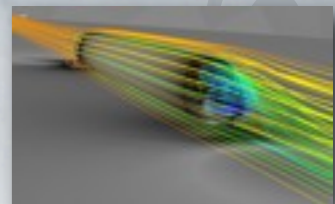
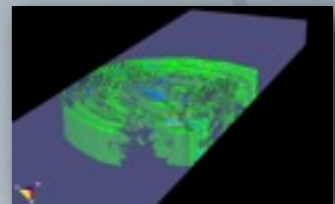
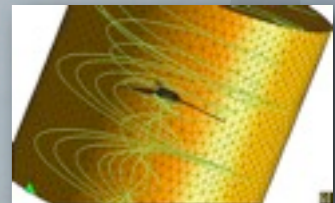
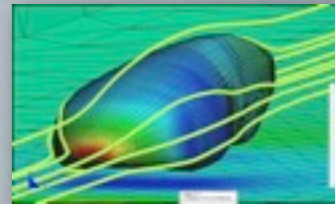
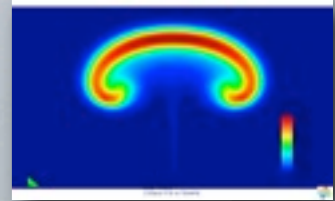
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ALYA (2004)

Simulation Code for parallel computing

Designed from scratch to solve multiphysics problems with high parallel efficiency

- * Numerical solution of PDE's**
- * Hybrid meshes, higher (up to Q3) and lower order**
- * Parallelization by MPI and OpenMP**
- * Automatic mesh partition using Metis**
- * Portability**



Services

Kernel

Modules

Multiphysics computational tool with high parallel efficiency

HPC-based

Supercomputing facilities

FEM method

Modules and services can be turned on/off

Solvers are in-house, no external libraries

Incompressible flows

Compressible flows

Turbulence

Non-linear Solid Mechanics

Electromagnetism

Heat transport

Combustion and chemical reactions

Arbitrary Lagrangian-Eulerian Fluid-Structure Interaction

Interaction

Adjoint-based optimization

HPC Simulation Tools: Alya

Alya is one of the two CFD codes of the PRACE benchmark suite

respective user communities, as well the coverage of scientific a
a final list of 12 codes to form the initial version of UEABS, whi

| | |
|-------------------|------------------------------|
| Particle Physics: | QCD |
| Classical MD: | NAMD, GROMACS |
| Quantum MD: | Quantum Espresso, CP2K, GPAW |
| CFD: | Code_Saturne, ALYA |
| Earth Sciences: | NEMO, SPECFEM3D |
| Plasma Physics: | GENE |
| Astrophysics: | GADGET |



Available online at www.prace-ri.eu

Partnership for Advanced Computing in Europe

Selection of a Unified European Application Benchmark Suite

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^bCINECA, via Magnanelli 6/3, 40033 Casalecchio di Reno, Bologna, Italy.

Lindgren (Sweden), Cray XE system at PDC, incompressible flow **12288** CPU's
(collaboration with Jing Gong from PDC)

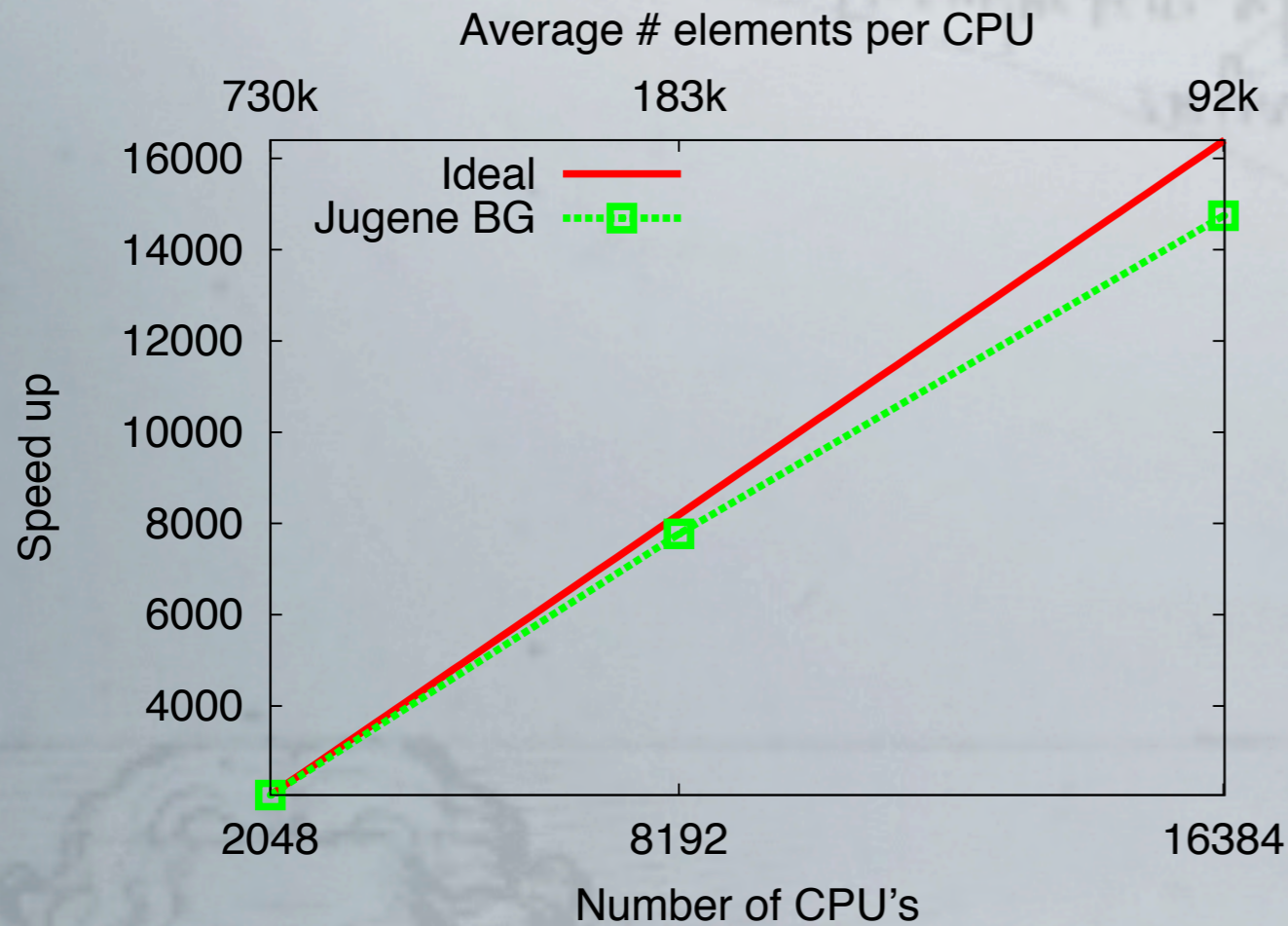
Huygens, (The Netherlands), IBM power 6, incompressible flow, **2128** CPU's

Jugene BG (Germany): **16384** CPU's, incompressible flow (Prace project for Mesh multiplication) and, running first tests of FSI in collaboration with Paolo Crosetto (Julich)

Fermi BG (Italy): **16384** CPU's, incompressible flow + species transport + Lagrangian particles (Prace project for nose)

Curie Bullx (France): **22528** CPU's, incompressible flow (collaboration with Jing Gong - PDC)

Marenostrum: **8000** CPU's compressible flow, incompressible flow, solid mechanics... (scalability test)



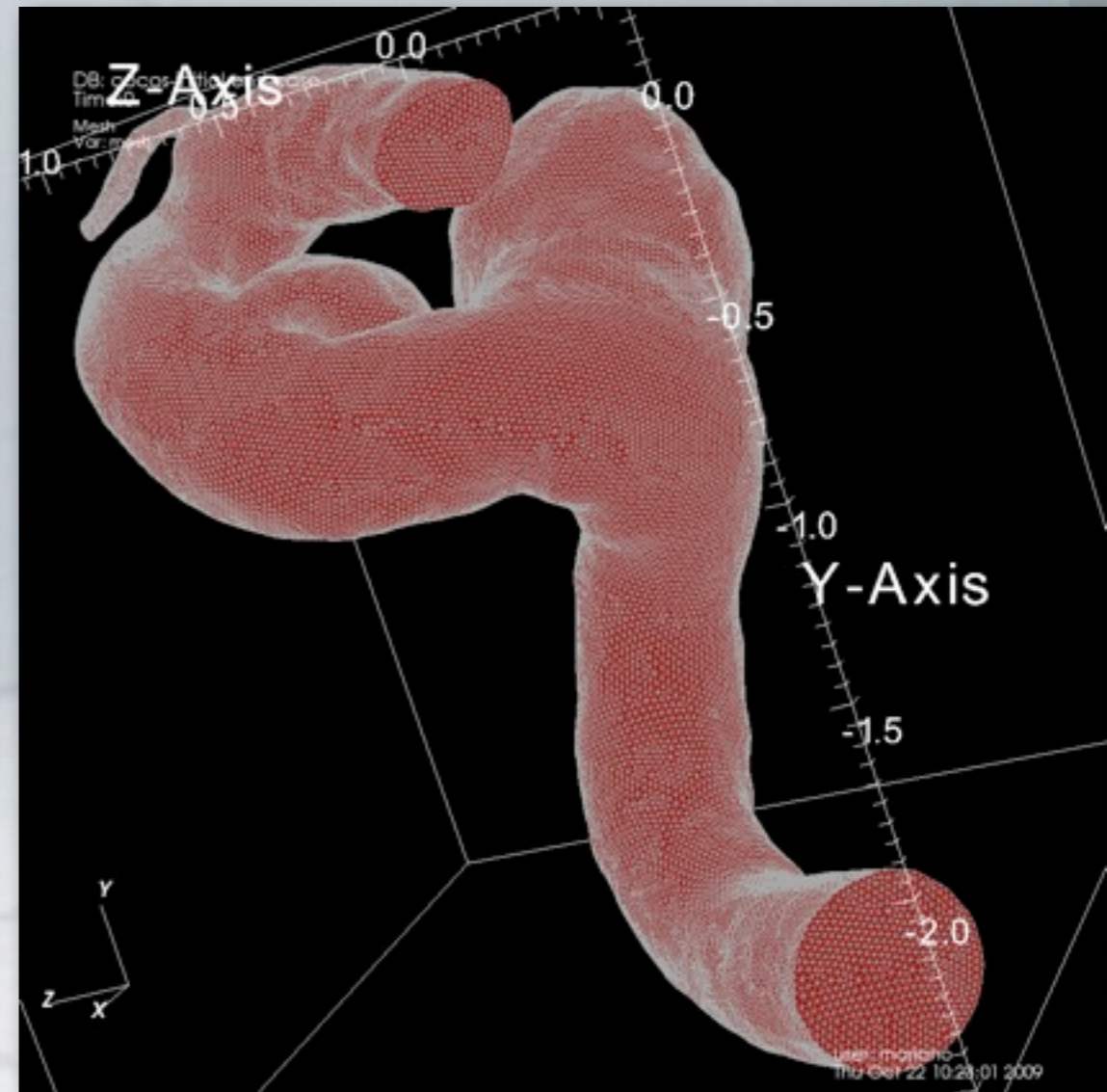
Benchmark

Aneurism geometry provided by R. Cebra
Uniform refinement up to 1.6B tetrahedra

Incompressible flow

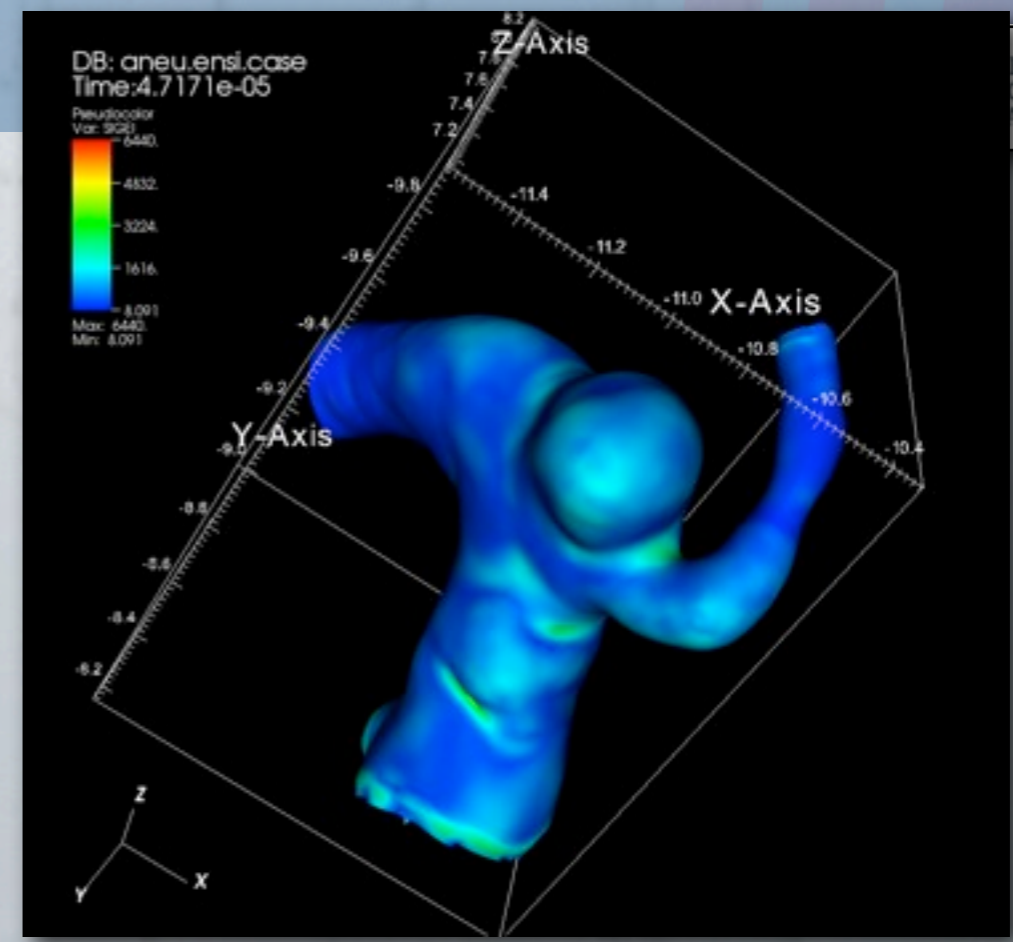
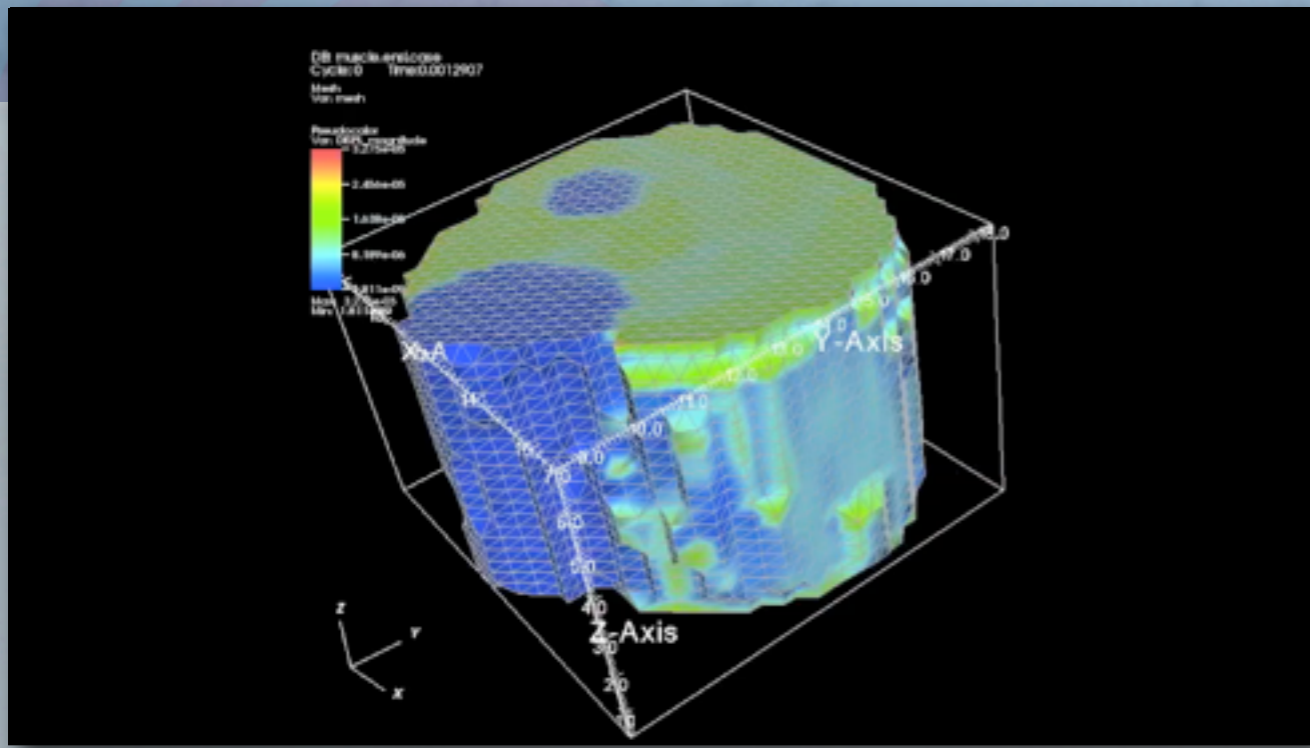
Implicit formulation

Algebraic Fractional Step: BCGStab + Deflated CG

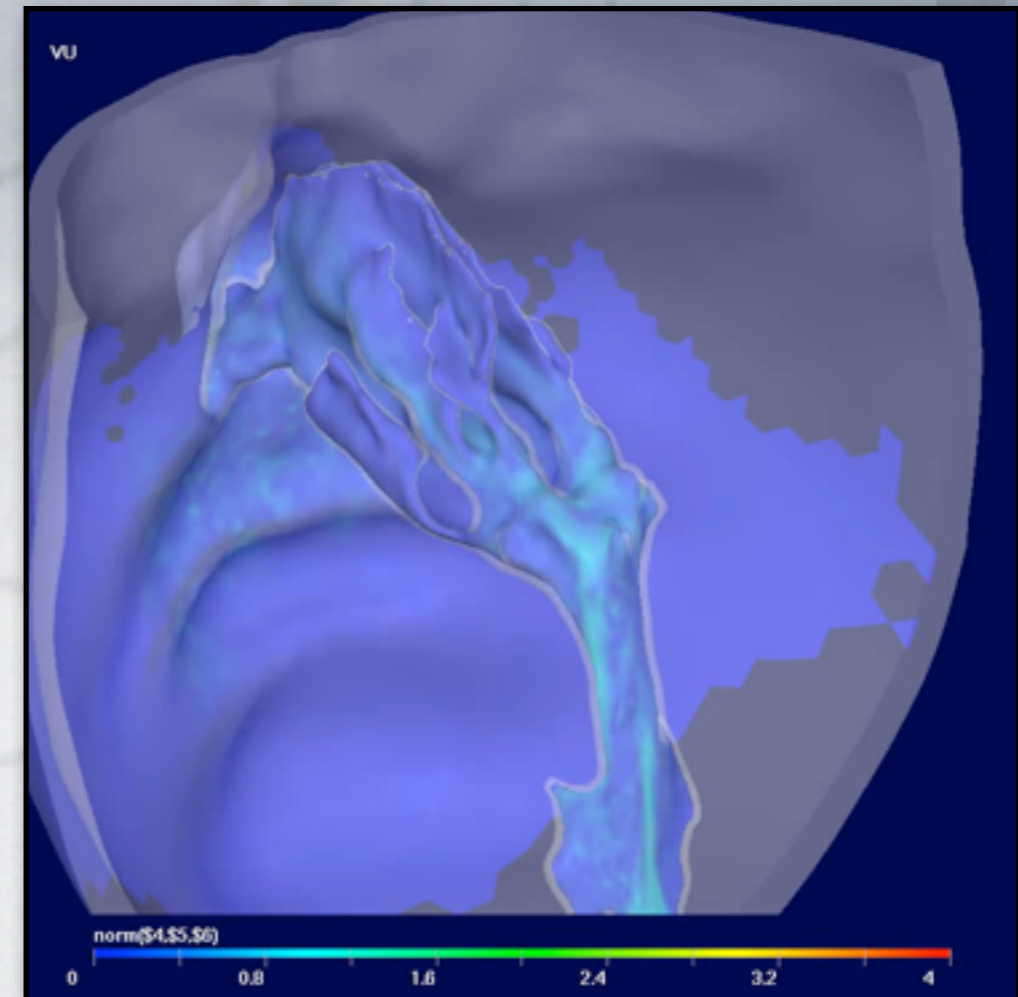
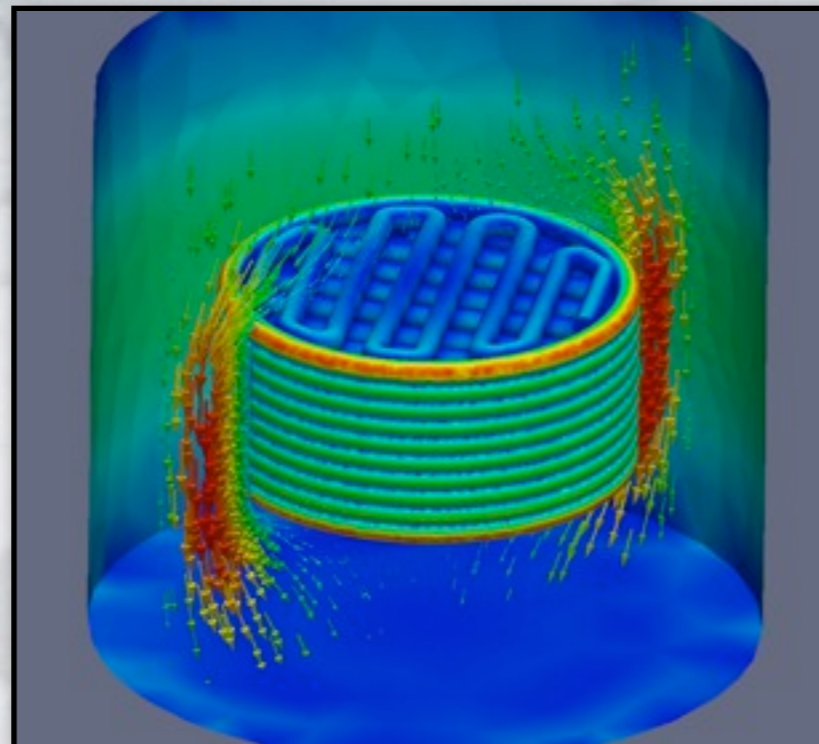


Alya Red

HPC-based Biomechanical Simulations



Respiratory system
 Cerebral aneurisms rupture risk
 Long skeletal muscles
 Biomaterials and tissue engineering
Cardiac computational model



The goal:
**Use of HPC-based simulation codes and HPC resources in
Biomedical research**



Alya Red: Cardiac Computational Model

Partially financed by the Severo Ochoa Excellence Program

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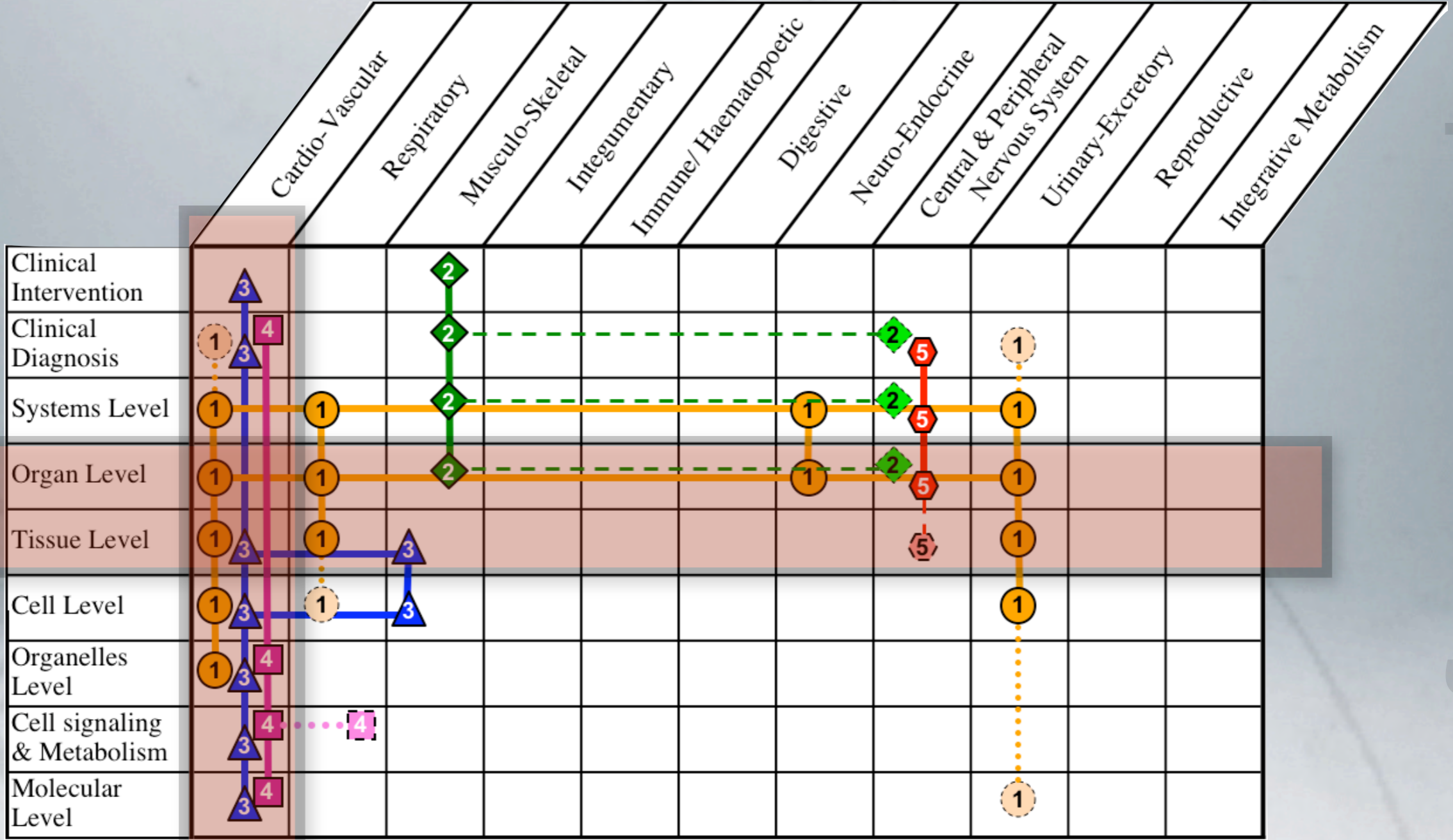
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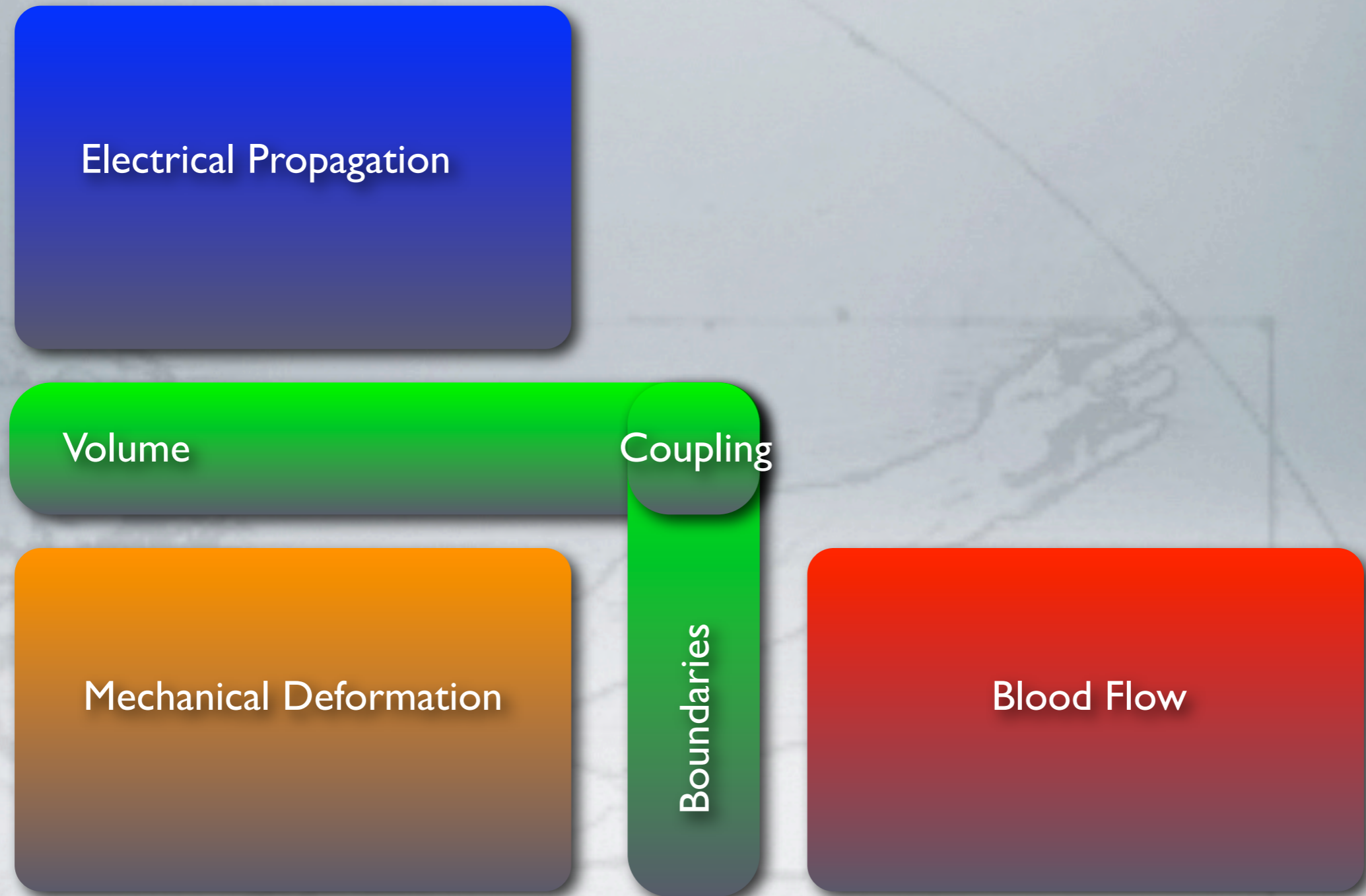
Pablo Lamata, Liya Asner and David
Nordsletten, King's College London
(UK)



Organ Systems vs. Levels of Organizations
 Extracted from S.R. Thomas et al., VPH Exemplar Project Strategy Document. Deliverable 9, VPH NoE. 2008

The Heart as a Physical System

At organ level,
the heart can be seen as the following coupled problem:



Electrical
Propagation

Electrophysiology:
Linear anisotropic (fibers) diffusion +
non-linear source terms

Volume

Electro-mechanical coupling, Ca^{2+} is the key

**ALE + Immersed
Boundaries**

Mechanical
Deformation

Boundaries

Blood Flow

Mechanical deformation:
Large deformations + non-linear material
models

**Incompressible
Flow**

- * **Four coupled problems:**

Electrophysiology, Solid Mechanics, Blood flow and Mesh deformation

- * **One single mesh for EP and CSM, one single mesh for CFD and MD**

- * **Non-structured mesh coming from medical image processing**

- * **Anisotropic media**

- * **One parallel code to simulate the full problem: Alya**

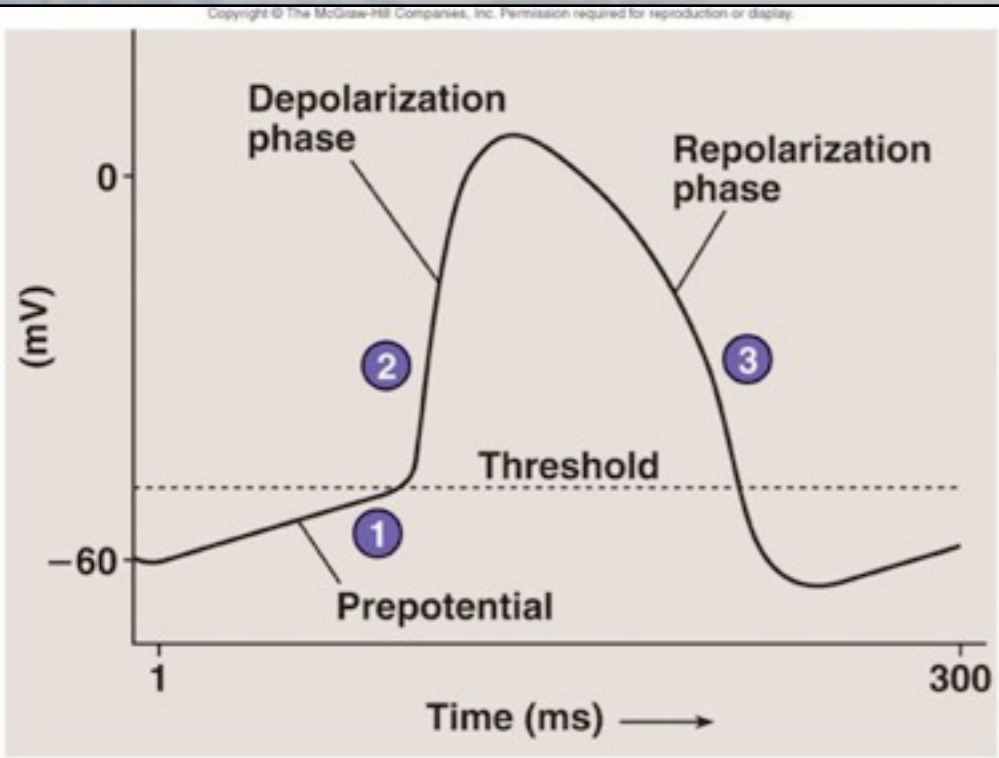
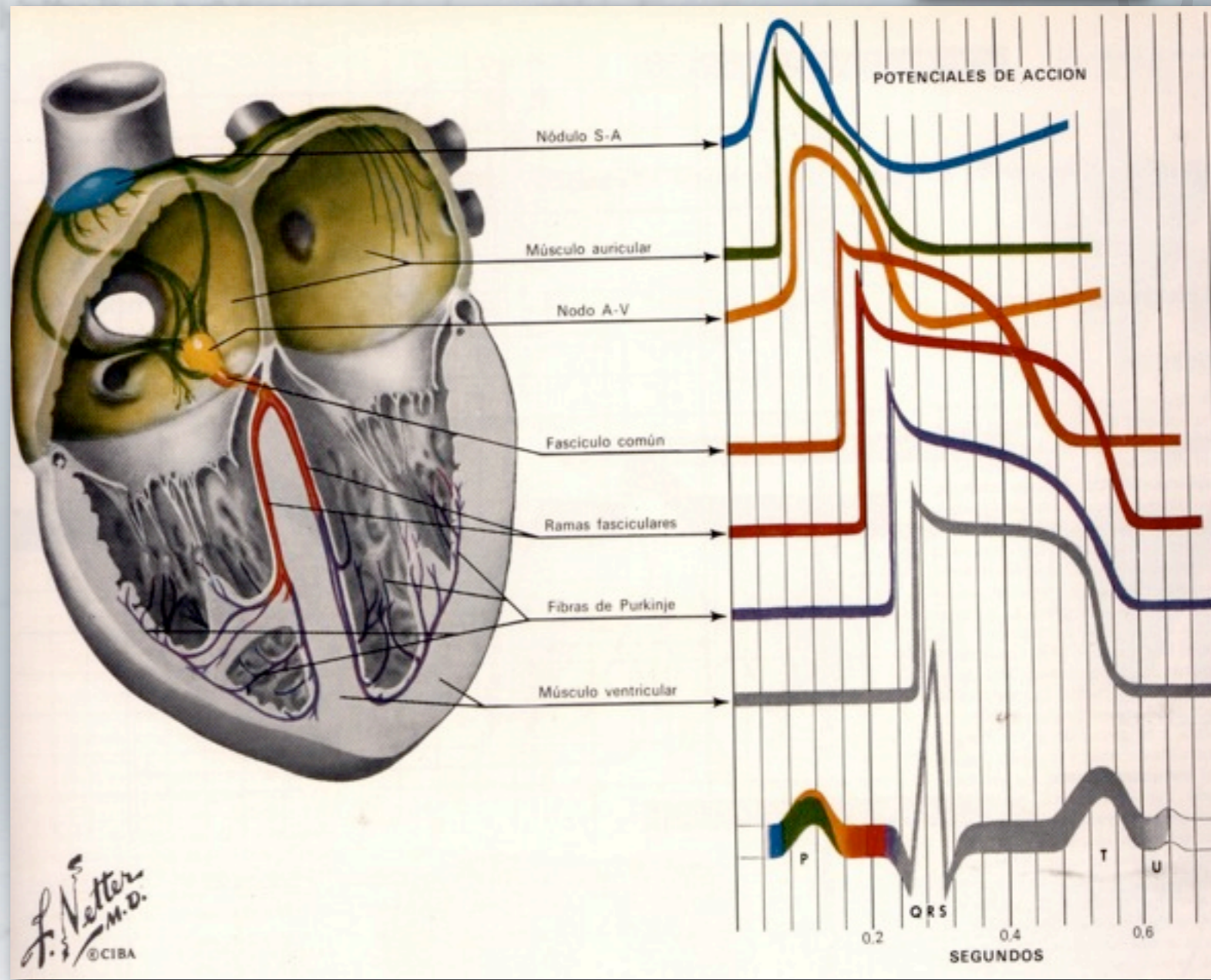
Staggered strategy: solving the problems sequentially for each time step

Eventually, allowing sub-iterations or sub-cycling, asynchronous strategies...

Fully transient (dynamic terms) problem

Diffusion equation + non-linear terms
 Supplementary Poisson equation (mono and bidomain)

Non-linear terms:
 FitzHugh-Nagumo, Fenton-Karma, Ten-Tuscher, O'Hara...



$$\frac{\partial \phi_\alpha}{\partial t} - \frac{\partial}{\partial x_i} \left(D_{ij} \frac{\partial \phi_\alpha}{\partial x_j} \right) = L(\phi_\alpha)$$

Electrophysiology

$$\frac{\partial \phi_\alpha}{\partial t} - \frac{\partial}{\partial x_i} \left(D_{ij} \frac{\partial \phi_\alpha}{\partial x_j} \right) = L(\phi_\alpha)$$

Phenomenological models based on Hodgkin-Huxley

FitzHugh-Nagumo model (1961)

$$L(\phi) = c_1 \phi(\phi - c_3)(\phi - 1) + c_2 W$$

$$\frac{\partial W}{\partial t} = \varepsilon(\phi - \gamma W)$$

Fenton-Karma model (2005)

$$L(\phi) = J_{fi}(\phi, V) + J_{so}(\phi) + J_{si}(\phi, W)$$

$$\frac{\partial V}{\partial t} = \Theta(\phi_c - \phi)(1 - V)/\tau_V^- - \Theta(\phi - \phi_c)V/\tau_V^+$$

$$\frac{\partial W}{\partial t} = \Theta(\phi_c - \phi)(1 - W)/\tau_W^- - \Theta(\phi - \phi_c)W/\tau_W^+$$

$$J_{fi}(\phi, V) = -\frac{V}{\tau_d} \Theta(\phi - \phi_c)(1 - \phi)(\phi - \phi_c)$$

$$J_{so}(\phi) = \frac{\phi}{\tau_0} \Theta(\phi_c - \phi) + \frac{1}{\tau_r} \Theta(\phi - \phi_c)$$

$$J_{si}(\phi, W) = -\frac{W}{2\tau_{si}} (1 + \tanh[k(\phi - \phi_c^{si})])$$

Cell models on ionic currents
Ten Tusscher - Noble - Panfilov

2005

Electrophysiology

$$h_{ca} = \frac{1}{[1 + e^{(V+71.55)/7.43}]^2} \quad (32)$$

$$\alpha_h = 0 \quad \text{if } V \geq -40 \quad (33)$$

$$\tau_h = \alpha_h + \beta_h \quad (34)$$

$$j_{ca} = \frac{1}{[1 + e^{(V+71.55)/7.43}]^2} \quad (35)$$

$$\alpha_j = 0 \quad \text{if } V \geq -40 \quad (36)$$

$$\alpha_j = \frac{(-2.5428 \times 10^4 e^{0.2444V} - 6.948) \times 10^{-6} e^{-0.04391V}}{1 + e^{0.311(V+79.23)}} \quad \text{otherwise} \quad (37)$$

$$\beta_j = \frac{0.6e^{0.057V}}{1 + e^{-0.1(V+32)}} \quad \text{if } V \geq -40 \quad (38)$$

$$\beta_j = \frac{0.02424e^{-0.01052V}}{1 + e^{-0.1378(V+40.14)}} \quad \text{otherwise} \quad (39)$$

$$\tau_j = \frac{1}{\alpha_j + \beta_j} \quad (39)$$

L-type Ca²⁺ Current

$$I_{CaL} = G_{CaL} df_{CaL} 4 \frac{VF^2}{RT} \frac{Ca_i e^{2VF/RT} - 0.341Ca_o}{e^{2VF/RT} - 1} \quad (40)$$

$$d_{ca} = \frac{1}{1 + e^{(-5-V)/7.5}} \quad (41)$$

$$\alpha_d = \frac{1.4}{1 + e^{(-35-V)/13}} + 0.25 \quad (42)$$

$$\beta_d = \frac{1.4}{1 + e^{(V+5)/5}} \quad (43)$$

$$\gamma_d = \frac{1}{1 + e^{(50-V)/20}} \quad (44)$$

$$\tau_d = \alpha_d \beta_d + \gamma_d \quad (45)$$

$$f_{ca} = \frac{1}{1 + e^{(V+20)/7}} \quad (46)$$

$$\tau_{ca} = 2 \text{ ms} \quad (47)$$

$$\tau_{fca} = 2 \text{ ms}$$

$$\frac{df_{ca}}{dt} = k \frac{f_{ca\infty} - f_{ca}}{\tau_{fca}}$$

$$k = 0 \quad \text{if } f_{ca\infty} > f_{ca} \quad \text{and } V > -60 \text{ mV}$$

$$k = 1 \quad \text{otherwise}$$

Transient Outward Current

$$I_{to} = G_{to} S(V - E_K) \quad (35)$$

For all cell types

$$r_{\infty} = \frac{1}{1 + e^{(20-V)/6}}$$

$$\tau_r = 9.5e^{-(V+40)/1800} + 0.8$$

For epicardial and M cells

$$s_{\infty} = \frac{1}{1 + e^{(V+20)/5}}$$

$$\tau_s = 85e^{-(V+45)/320} + \frac{5}{1 + e^{(V-20)/5}} + 3$$

For endocardial cells

$$s_{\infty} = \frac{1}{1 + e^{(V+28)/5}}$$

$$\tau_s = 1,000e^{-(V+67)/1,000} + 8$$

Slow Delayed Rectifier Current

$$I_{Ks} = G_{Ks} x_{r1}^2 (V - E_{Ks})$$

$$x_{r\infty} = \frac{1}{1 + e^{(-5-V)/14}}$$

$$\alpha_{x1} = \frac{1,100}{\sqrt{1 + e^{(-10-V)/6}}}$$

$$\beta_{x1} = \frac{1}{1 + e^{(V-60)/20}}$$

$$\tau_{x1} = \alpha_{x1} \beta_{x1}$$

Rapid Delayed Rectifier Current

$$I_{Kr} = G_{Kr} \sqrt{\frac{K_o}{5.4}} x_{r1} x_{r2} (V - E_K)$$

$$x_{r1\infty} = \frac{1}{1 + e^{(-26-V)/7}}$$

$$\alpha_{x1} = \frac{450}{1 + e^{(-45-V)/10}}$$

Inward Rectifier K⁺ Current

$$I_{K1} = G_{K1} \sqrt{\frac{K_o}{5.4}} x_{K1\infty} (V - E_K)$$

$$\alpha_{K1} = \frac{0.1}{1 + e^{0.06(V-E_K-200)}}$$

$$\beta_{K1} = \frac{3e^{0.0002(V-E_K+100)} + e^{0.1(V-E_K-10)}}{1 + e^{-0.5(V-E_K)}}$$

$$x_{K1\infty} = \frac{\alpha_{K1}}{\alpha_{K1} + \beta_{K1}}$$

Na⁺/Ca²⁺ Exchanger Current

$$I_{NaCa} = k_{NaCa} \frac{e^{\gamma VF/RT} Na_i^3 Ca_o - e^{(\gamma-1)VF/RT} Na_o^3 Ca_i \gamma}{(K_{mNa}^3 + Na_o^3)(K_{mCa} + Ca_o)(1 + k_{sr} e^{(\gamma-1)VF/RT})}$$

Na⁺/K⁺ Pump Current

$$I_{NaK} = P_{NaK} \frac{K_o Na_i}{(K_o + K_{mK})(Na_i + K_{mNa})(1 + 0.1245e^{-0.1VF/RT} + 0.0353e^{-0.1VF/RT})}$$

I_{pCa}

$$I_{pCa} = G_{pCa} \frac{Ca_i}{K_{pCa} + Ca_i}$$

I_{pK}

$$I_{pK} = G_{pK} \frac{V - E_K}{1 + e^{(25-V)/5.98}}$$

Background Currents

$$I_{bNa} = G_{bNa} (V - E_{Na})$$

$$I_{bCa} = G_{bCa} (V - E_{Ca})$$

Calcium Dynamics

$$I_{leak} = V_{leak} (Ca_{sr} - Ca_i)$$

$$I_{up} = \frac{V_{maxup}}{1 + K_{up}^2 / Ca_i^2}$$

$$I_{rel} = \left(a_{rel} \frac{Ca_{sr}^2}{b_{rel}^2 + Ca_{sr}^2} + c_{rel} \right) dg$$

$$g_{\infty} = \frac{1}{1 + Ca_i^6 / 0.00035^6} \quad \text{if } Ca_i \leq 0.00035$$

$$g_{\infty} = \frac{1}{1 + Ca_i^6 / 0.00035^6} \quad \text{otherwise}$$

Mechanical deformation: Material model

Mechanical properties of the cardiac tissue are defined through the Cauchy stress

$$\boldsymbol{\sigma} = J^{-1} \mathbf{P} \mathbf{F}^T$$

Stress is composed by passive and active parts

$$\boldsymbol{\sigma} = \boldsymbol{\sigma}_{pas} + \sigma_{act}(\lambda, [Ca^{2+}]) \mathbf{f} \otimes \mathbf{f}$$

Passive stress + Active stress

Material Models based on biaxial testing of excised myocardium
(Lin & Yin, 1998)

Passive stress is (based on Holtzapfel 2009, but compressible and transversally isotropic)

$$\begin{aligned} J \boldsymbol{\sigma}_{pas} = & (a e^{b(I_1 - 3)} - a) \mathbf{b} + 2a_f (I_4 - 1) e^{b_f (I_4 - 1)^2} \bar{\mathbf{f}} \otimes \bar{\mathbf{f}} \\ & + K (J - 1) \mathbf{I} \end{aligned}$$

Mechanical deformation: Coupling

Active stress is (Hunter and co-workers)

$$\sigma_{act} = \alpha \frac{[Ca^{2+}]^n}{[Ca^{2+}]^n + C_{50}^n} \sigma_{max} (1 + \beta(\lambda_f - 1))$$

where free calcium concentration comes from the chosen EP model.

α controls the strength of the coupling.

Synthetic Purkinje System

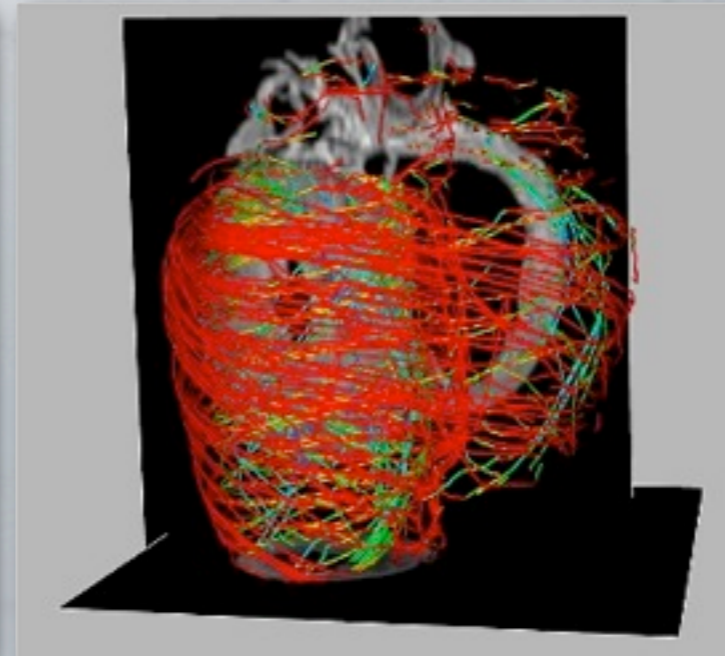
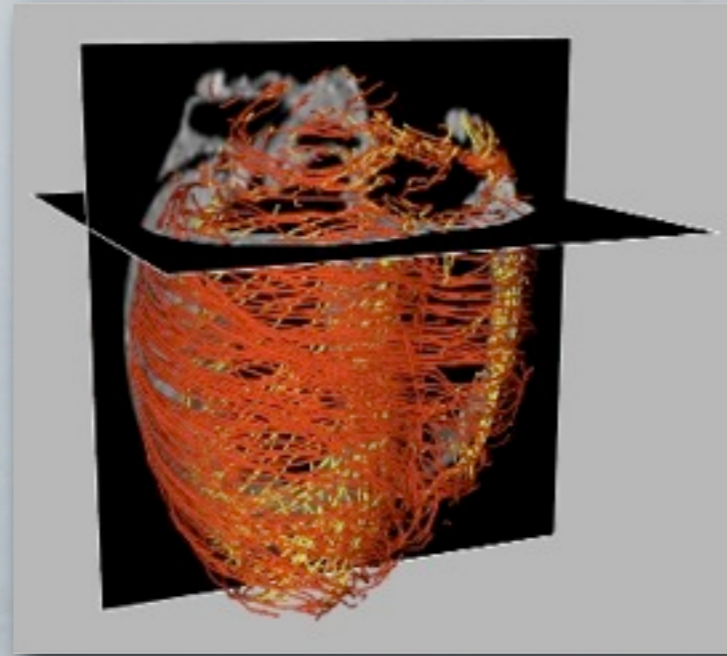
Electrical propagation through the Purkinje system.
It delivers the initial impulse.



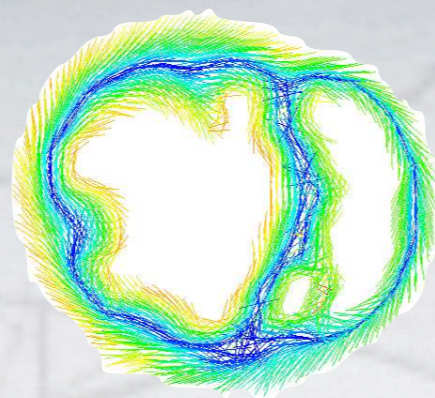
Sebastian R. et al.

Characterization and Modeling of the Peripheral Cardiac Conduction System, 2012.

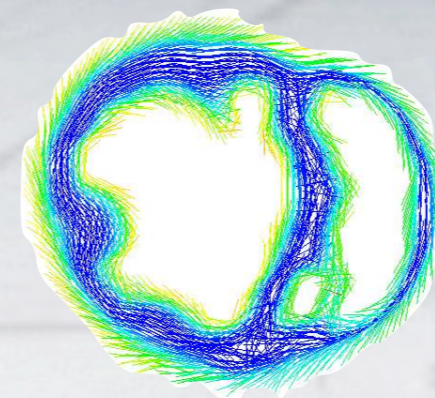
DTI (Ex-vivo and In-vivo)



Anisotropic fiber model: Rule-based (Streeter)



Linear Model

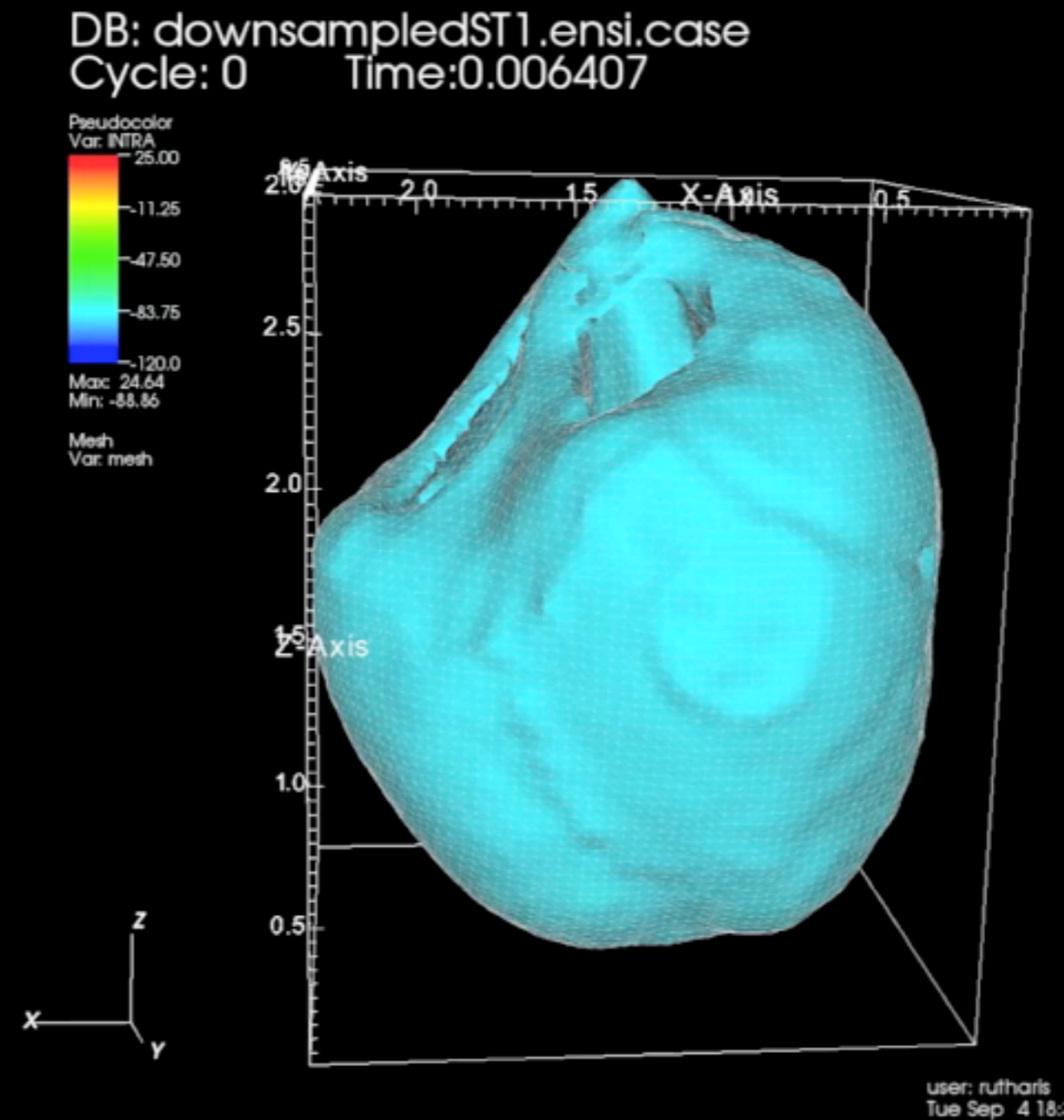
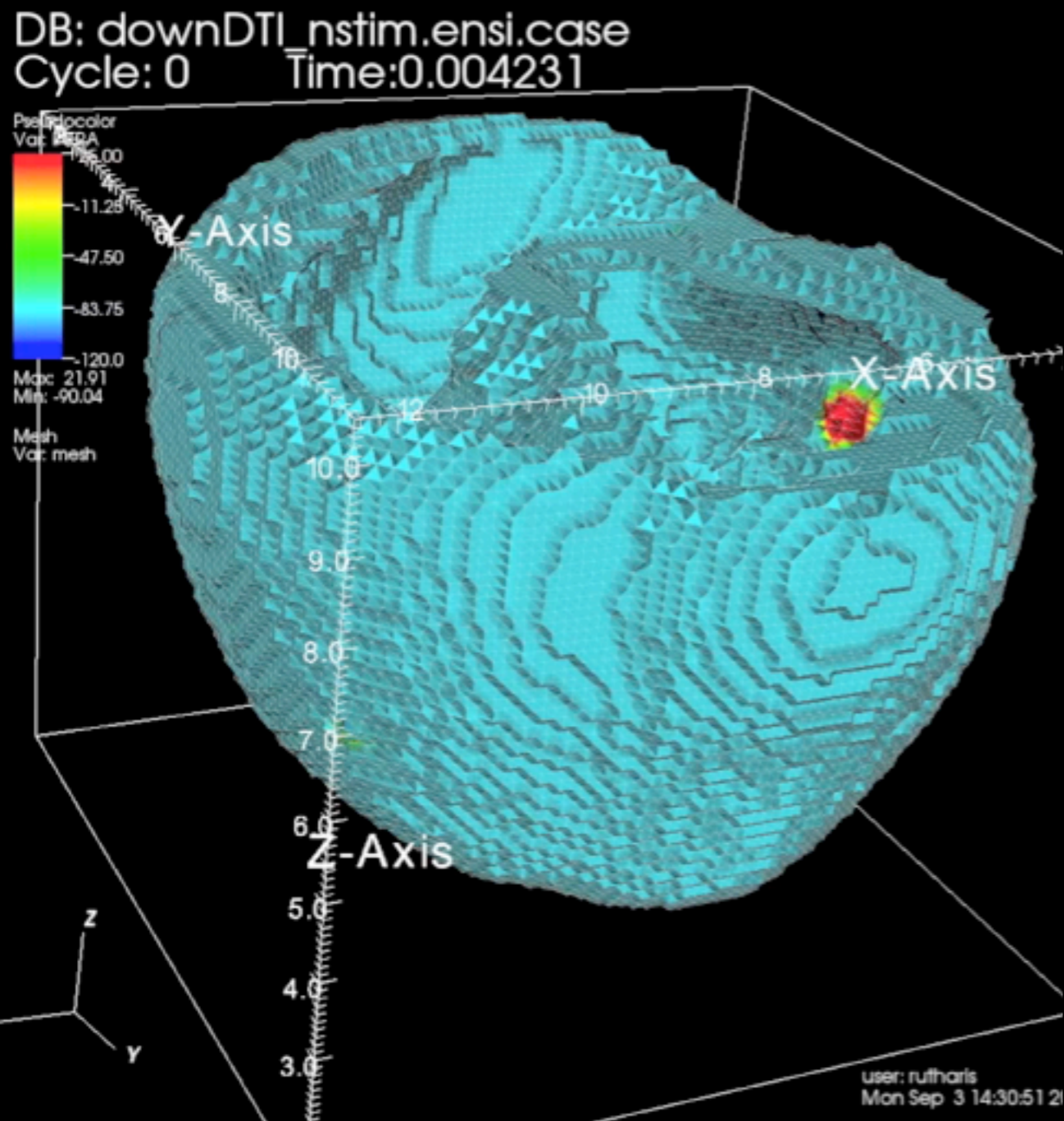


Cubic Model

Fiber orientation: Rule-Based approach (Potse et al., 2006)

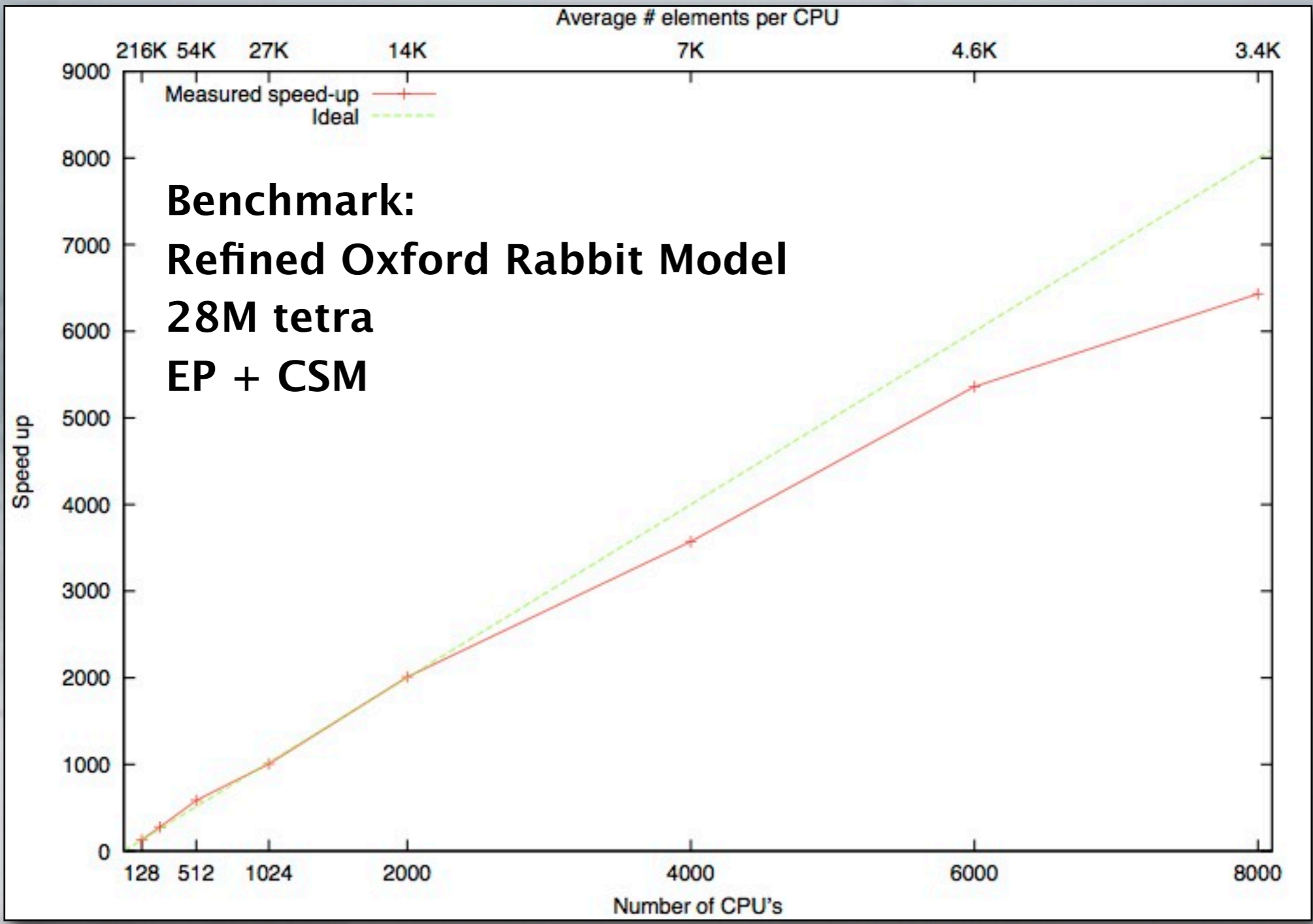
Dog (Johns Hopkins University)

Rabbit (University of Oxford)



Electromechanical Coupling:
Electrical Activation + Mechanical Deformation

Scalability: Electro - Mechanical problem Marenstrum III - BSC



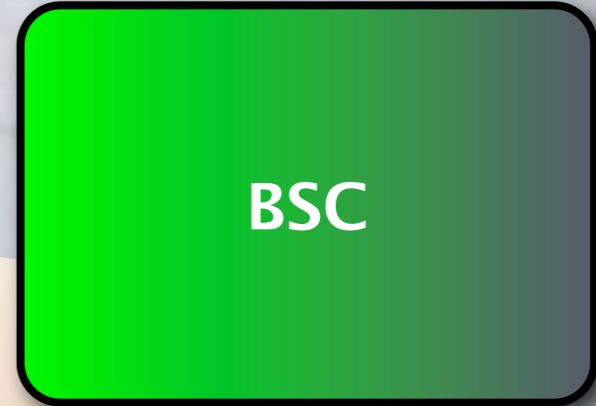
BSC – KCL



Cardiologists:

Understanding biological systems
Physiological models

They provide the main motivation and insight to the problem



Computational scientists:

Developing computational tools to run simulations

Provide the required simulation capacity

High Performance Computational Mechanics

Bio-mechanics researchers:

Develop the Physiological models
Deal with medical image processing
Design data acquisition tools

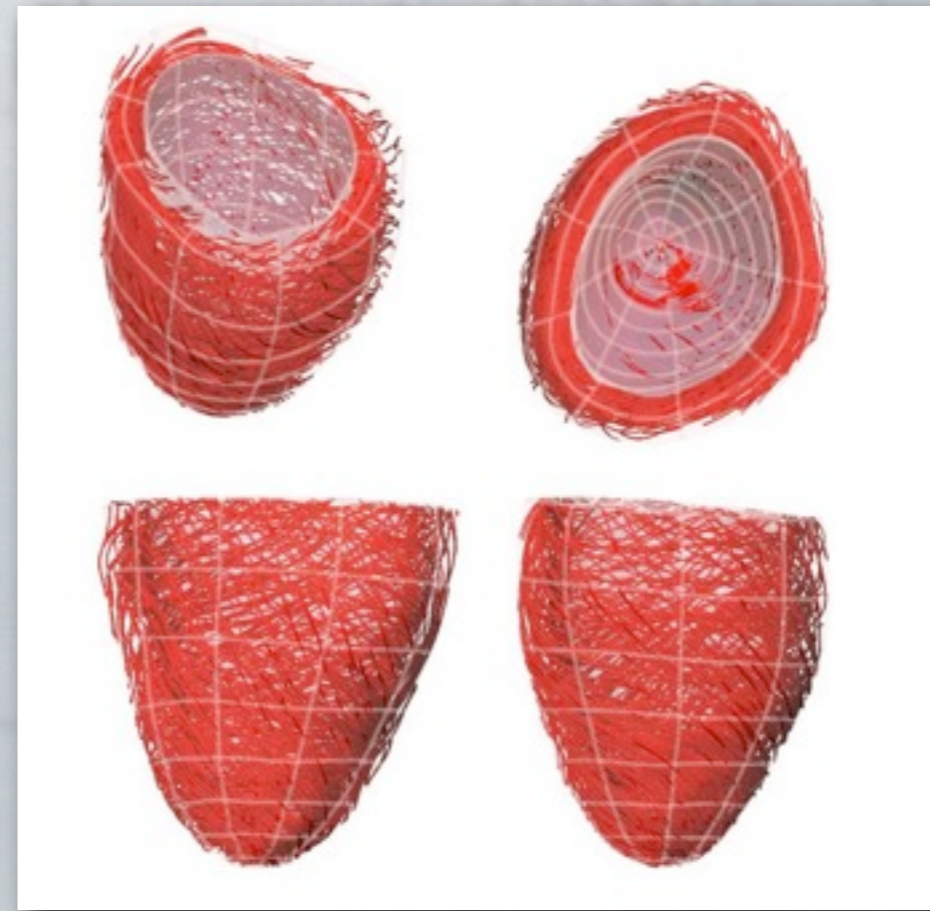




St Thoma's Hospital

Pablo Lamata, Liya Asner
and David Nordsletten

Cardiac Image (LV)
+
Fibers (DTI)



Human LV
Code: CHeart

$$W = C_1 e^{AC_2 + BC_3 + DC_4}$$

$$\alpha = C_1 + C_2 + C_3$$

$$r_3 = \frac{C_3}{\alpha}$$

$$r_4 = \frac{C_4}{\alpha}$$

Functional to characterize the minimum:
Averaged distance between equivalent Gauss point
of the reference and simulated

$$J_i(x_i, y_i) = \sqrt{\frac{1}{G} \sum_g \|x_{ig} - y_{ig}\|^2}$$

Forward Model:

* C_1 — α space

* r_3 — r_4 space

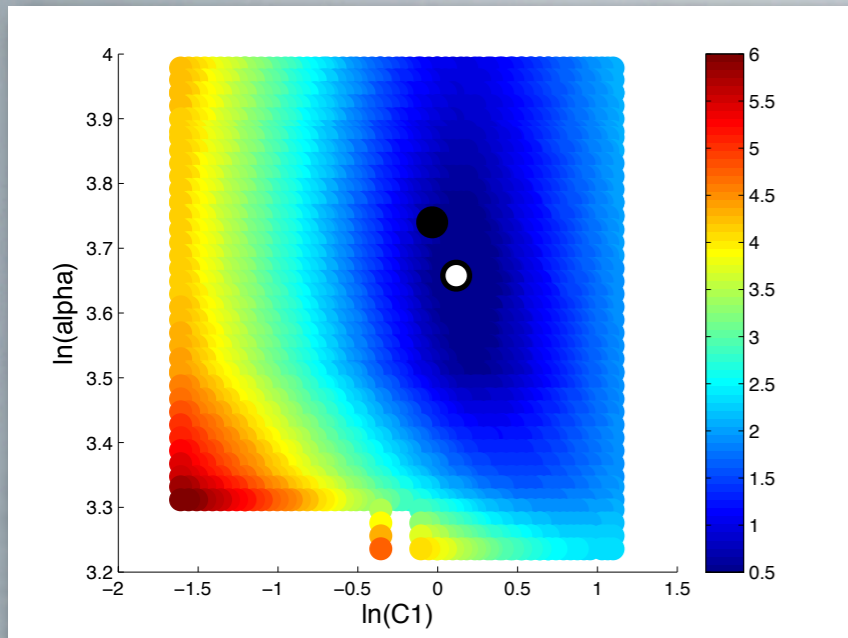
$$W = C_1 e^{AC_2 + BC_3 + DC_4}$$

$$\alpha = C_1 + C_2 + C_3$$

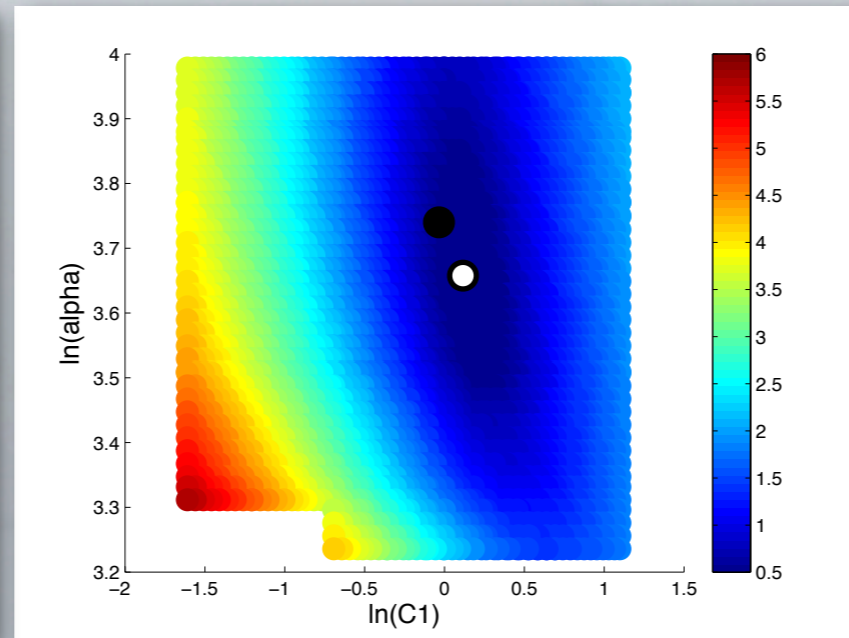
$$r_3 = \frac{C_3}{\alpha}$$

$$r_4 = \frac{C_4}{\alpha}$$

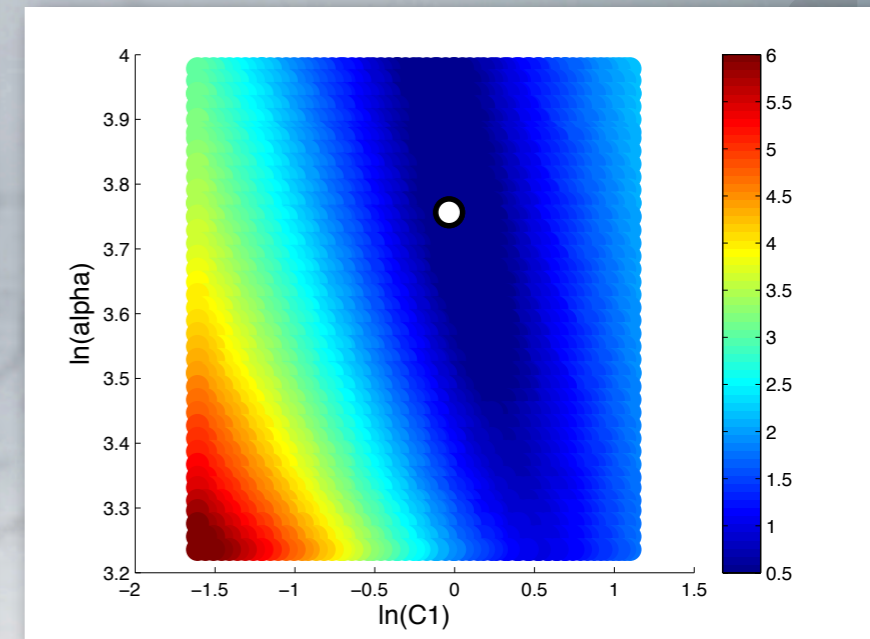
$$C_1 - \alpha$$



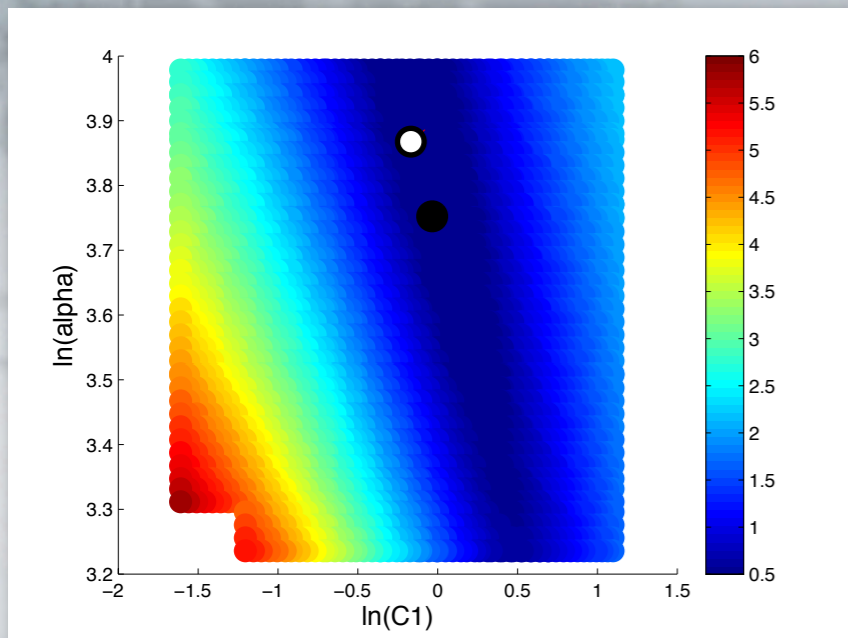
Angle 0



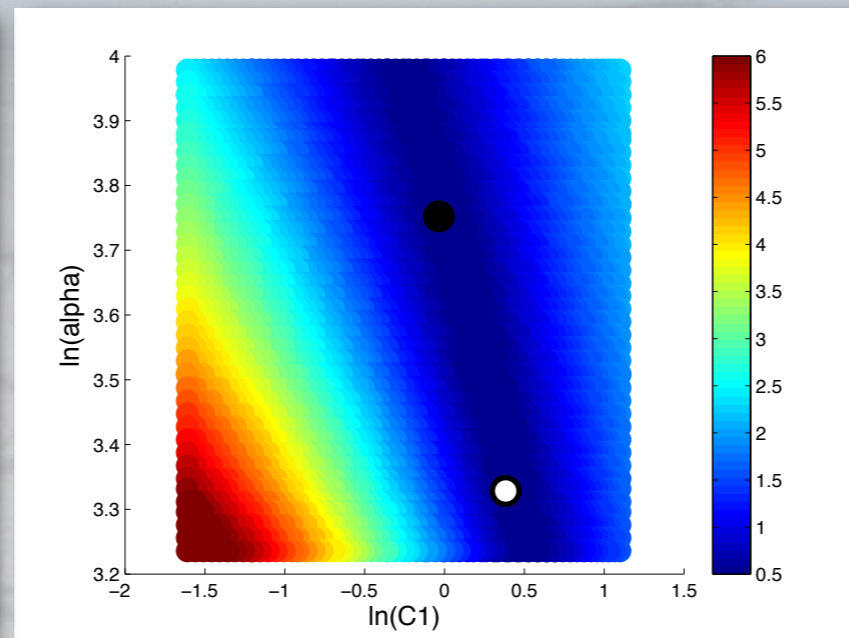
Angle 30



DTI

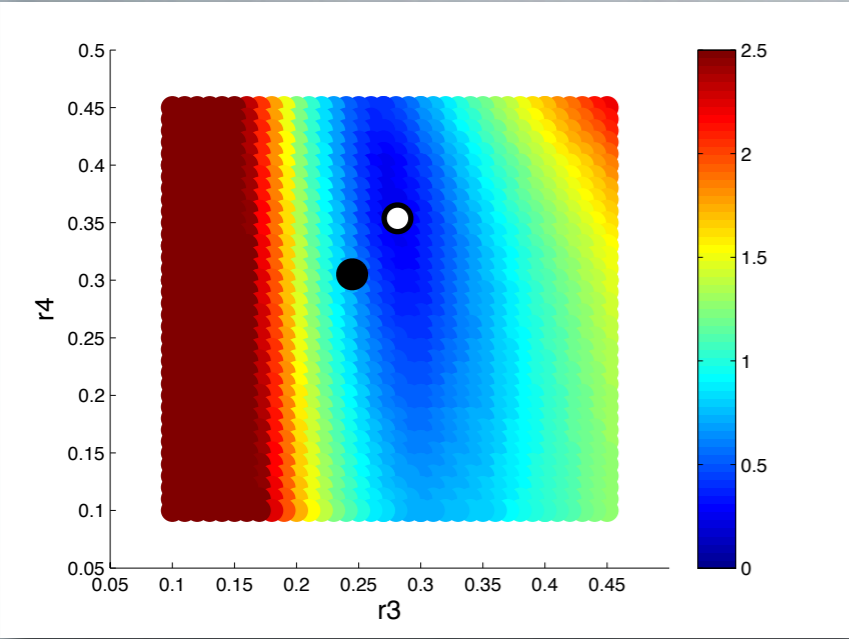


Angle 60

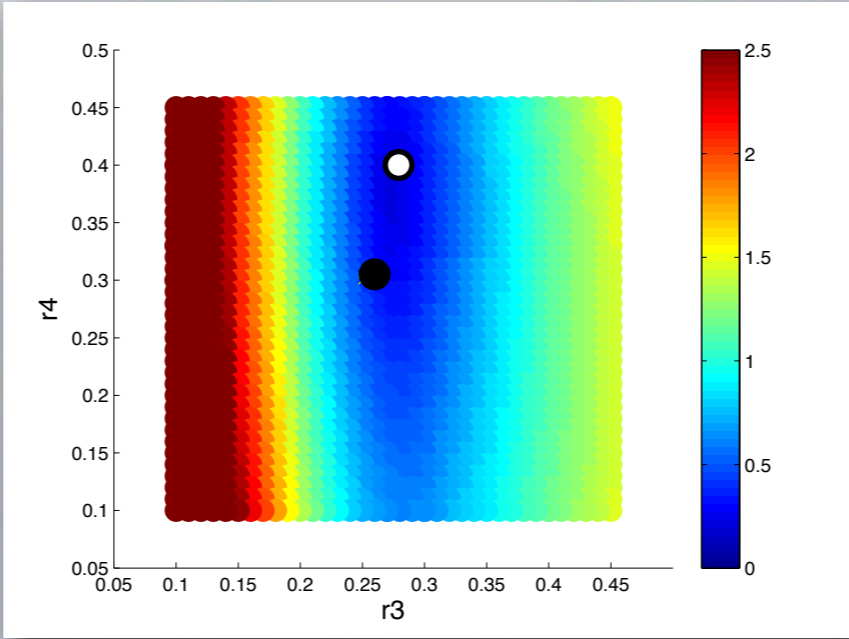


Angle 90

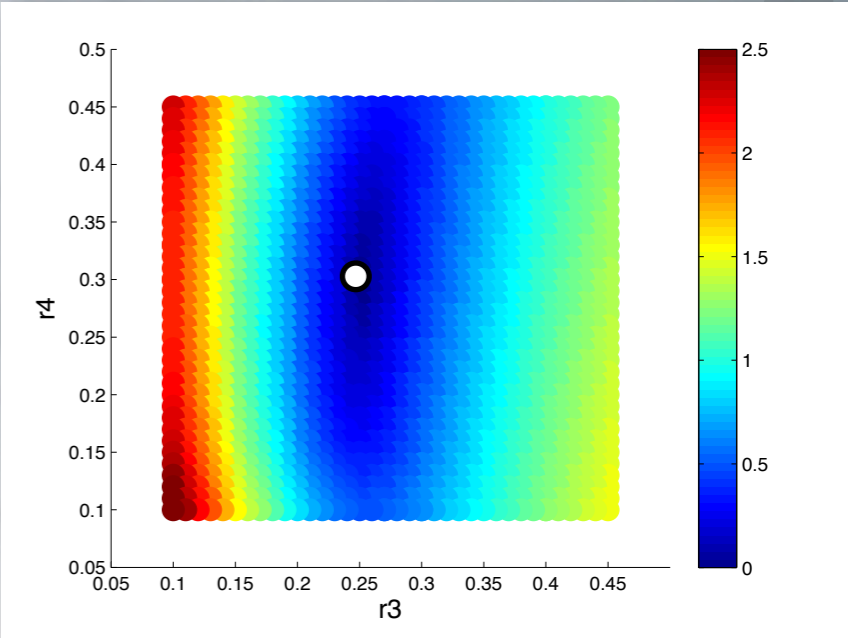
$$r_3 - r_4$$



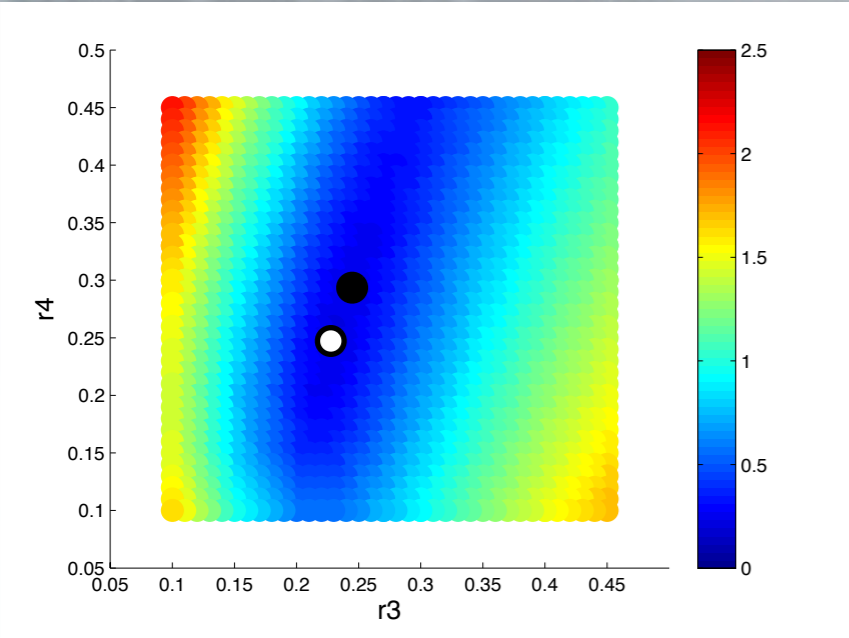
Angle 0



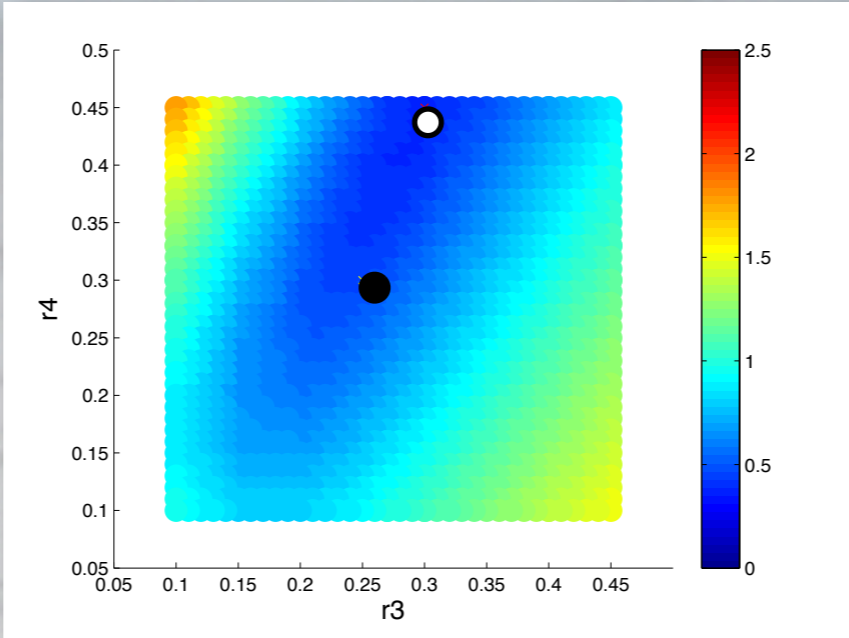
Angle 30



DTI



Angle 60



Angle 90



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Spain

